## LISTING OF THE CLAIMS

## CLAIMS

What is claimed is:

- (Original) A method of detecting a fracture with residual width from a previous well treatment during a well fracturing operation in a subterranean formation containing a reservoir fluid, comprising the steps of:
- (a) injecting an injection fluid into the formation at an injection pressure exceeding the formation fracture pressure;
- (b) gathering pressure measurement data from the formation during the injection and a subsequent shut-in period;
- (c) transforming the pressure measurement data into a constant rate equivalent pressure; and
- (d) detecting the presence of a dual unit-slope wellbore storage in the transformed pressure measurement data, said dual unit-slope being indicative of the presence of a fracture retaining residual width.
- (Original) The method of claim 1 wherein the time of injection is limited to the time required for the reservoir fluid to exhibit pseudoradial flow.
- 3. (Original) The method of claim 1 wherein

the reservoir fluid is compressible; and

the transformation of pressure measurement data is based on the properties of the compressible fluid contained in the reservoir.

- 4. (Original) The method of claim 3 wherein the transforming step comprises the step of calculating:
- a shut-in time relative to the end of the injection:  $\Delta t = t t_{ne}$ ;
- an adjusted time:  $t_a = (\overline{\mu c_t}) \int_0^{\Delta t} \frac{d\Delta t}{(\mu c_t)_w}$ ; and

- an adjusted pseudo pressure difference:  $\Delta p_a(t) = p_{aw}(t) - p_{ai}$  where  $p_a = \frac{\overline{\mu}_g \overline{z}}{\overline{p}} \int_0^p \frac{p dp}{\mu_g z}$ ;

wherein:

 $t_{ne}$  is the time at the end of injection;

 $\bar{\mu}$  is the viscosity of the reservoir fluid at average reservoir pressure;

 $(\mu c_t)_w$  is the viscosity compressibility product of wellbore fluid at time t;

 $(\mu c_t)_0$  is the viscosity compressibility product of wellbore fluid at time  $t = t_{ne}$ ;

p is the pressure;

 $\overline{p}$  is the average reservoir pressure;

 $p_{aw}(t)$  is the adjusted pressure at time t;

 $p_{at}$  is the adjusted pressure at time  $t = t_{ne}$ ;

c, is the total compressibility;

 $\overline{c}_t$  is the total compressibility at average reservoir pressure; and

z is the real gas deviator factor.

5. (Original) The method of claim 4 further comprising the step of plotting a log-log graph of a pressure function versus time:  $I(\Delta p_a) = f(t_a)$ ;

where 
$$I(\Delta p_a) = \int_0^{t_a} \Delta p_a dt_a$$
.

6. (Original) The method of claim 4 further comprising the step of plotting a log-log graph of a pressure derivative function versus time:  $\Delta p_a' = f(t_a)$ ;

where 
$$\Delta p_a' = \frac{d(\Delta p_a)}{d(\ln t_a)} = \Delta p_a t_a$$
.

- (Original) The method of claim 3 wherein the injection fluid is slightly compressible and contains desirable additives for compatibility with said formation.
- (Original) The method of claim 3 wherein the injection fluid is compressible and contains desirable additives for compatibility with said formation.

9. (Original) The method of clam 1 wherein

the reservoir fluid is slightly compressible; and

the transformation of pressure measurement data is based on the properties of the slightly compressible fluid contained in the reservoir.

- 10. (Original) The method of claim 9 wherein the transforming step comprises the step of calculating:
- a shut-in time relative to the end of the injection:  $\Delta t = t t_{ne}$ ; and
- a pressure difference:  $\Delta p(t) = p_w(t) p_i$ ;

wherein:

 $t_{ne}$  is the time at the end of injection;

 $p_w(t)$  is the pressure at time t; and

 $p_i$  is the initial pressure at time  $t = t_{ne}$ .

11. (Original) The method of claim 10 further comprising the step of plotting a log-log graph of a pressure function versus time:  $I(\Delta p) = I(\Delta t)$ ;

where 
$$I(\Delta p) = \int_0^{\Delta t} \Delta p d\Delta t$$
.

12. (Original) The method of claim 10 further comprising the step of plotting a log-log graph of a pressure derivatives function versus time:  $\Delta p' = f(\Delta t)$ ;

where 
$$\Delta p' = \frac{d(\Delta p)}{d(\ln \Delta t)} = \Delta p \Delta t$$
.

- 13. (Original) The method of claim 9 wherein the injection fluid is compressible and contains desirable additives for compatibility with said formation.
- 14. (Original) The method of claim 9 wherein the injection fluid is slightly compressible and contains desirable additives for compatibility with said formation.

- 15. (Original) A system for detecting a fracture with residual width from a previous well treatment during a well fracturing operation in a subterranean formation containing a reservoir fluid, comprising:
- a pump for injecting an injection fluid at an injection pressure exceeding the formation fracture pressure;
- means for gathering pressure measurement data in the wellbore at various points in time during the injection and a subsequent shut-in period;
- processing means for transforming said pressure measurement data into a constant rate equivalent pressure; and
- means for detecting the presence of a dual unit-slope wellbore storage in the transformed pressure measurement data, said dual unit-slope being indicative of the presence of a fracture retaining residual width.
- 16. (Original) The system of claim 15 wherein the processing means comprises graphics means for plotting said transformed pressure measurement data.
- 17. (Original) The system of claim 15 wherein the time of injection of said injecting means is limited to the time required for the reservoir fluid to exhibit pseudoradial flow.
- 18. (Original) The system of claim 15 wherein:

the reservoir fluid is compressible; and

the transformation of pressure measurement data is based on the properties of the compressible reservoir fluid.

- 19. (Original) The system of claim 18 wherein the transformed data are obtained by calculating:
- a shut-in time relative to the end of the injection:  $\Delta t = t t_{ne}$ ;

- an adjusted time: 
$$t_a = (\overline{\mu c_t}) \int_0^{\Delta t} \frac{d\Delta t}{(\mu c_t)_w}$$
; and

- an adjusted pseudo pressure difference:  $\Delta p_a(t) = p_{aw}(t) - p_{ai}$  where  $p_a = \frac{\overline{\mu}_g \overline{z}}{\overline{p}} \int_0^p \frac{p dp}{\mu_e z}$ ;

wherein:

 $t_{ne}$  is the time at the end of injection;

 $\bar{\mu}$  is the viscosity of the reservoir fluid at average reservoir pressure;

 $(\mu c_t)_w$  is the viscosity compressibility product of wellbore fluid at time t;

 $(\mu c_t)_0$  is the viscosity compressibility product of wellbore fluid at time  $t = t_{ne}$ ;

p is the pressure;

 $\overline{p}$  is the average reservoir pressure;

 $p_{ow}(t)$  is the pressure at time t;

 $p_{al}$  is the pressure at time  $t = t_{ne}$ ;

 $c_t$  is the total compressibility;

 $\overline{c}_t$  is the total compressibility at average reservoir pressure; and

z is the real gas deviator factor.

20. (Original) The system of claim 19 further comprising graphic means for plotting a log-log graph of a pressure function versus time:  $I(\Delta p_a) = f(t_a)$ ;

where  $I(\Delta p_a) = \int_0^{t_a} \Delta p_a dt_a$ .

21. (Original) The system of claim 19 further comprising graphic means for plotting a log-log graph of a pressure derivative function versus time:  $\Delta p_a' = f(t_a)$ ;

where 
$$\Delta p_a' = \frac{d(\Delta p_a)}{d(\ln t_a)} = \Delta p_a t_a$$
.

- 22. (Original) The system of claim 15 wherein the injection fluid is compressible and contains desirable additives for compatibility with said formation.
- 23. (Original) The system of claim 15 wherein the injection fluid is slightly compressible and contains desirable additives for compatibility with said formation.

24. (Original) The system of claim 15 wherein:

the reservoir fluid is slightly compressible; and

the transformation of pressure measurement data is based on the properties of the slightly compressible reservoir fluid.

- 25. (Original) The system of claim 24 wherein the transformed data are obtained by calculating:
- a shut-in time relative to the end of the injection:  $\Delta t = t t_{ne}$ ;
- a pressure difference:  $\Delta p(t) = p_w(t) p_i$ ;

wherein:

 $t_{ne}$  is the time at the end of injection;

 $p_w(t)$  is the pressure at time t; and

 $p_i$  is the initial pressure at time  $t = t_{ne}$ .

26. (Original) The system of claim 25 further comprising graphic means for plotting a log-log graph of a pressure function versus time:  $I(\Delta p) = f(\Delta t)$ ;

where  $I(\Delta p) = \int_0^{\Delta t} \Delta p d\Delta t$ .

27. (Original) The system of claim 25 further comprising graphic means for plotting a log-log graph of a pressure derivatives function versus time:  $\Delta p' = f(\Delta t)$ ;

where 
$$\Delta p' = \frac{d(\Delta p)}{d(\ln \Delta t)} = \Delta p \Delta t$$
.

- 28. (Original) A system for detecting a fracture with residual width from previous well treatment during a well fracturing operation in a subterranean formation containing a reservoir fluid, comprising:
- a pump for injecting an injection fluid at an injection pressure exceeding the formation fracture pressure;
- means for gathering pressure measurement data in the wellbore at various points in time during the injection and a subsequent shut-in period;
- processing means for transforming said pressure measurement data into a constant rate equivalent pressure; and
- graphics means for plotting said transformed pressure measurement data representative of before and after closure periods of wellbore storage, and for detecting a dual unit-slope wellbore storage indicative of the presence of a fracture retaining residual width.

## 29. (Original) The system of claim 28 wherein

- the reservoir fluid is compressible;
- the injection fluid is compressible or slightly compressible and contains desirable additives for compatibility with said formation; and
- the transformation of pressure measurement data is based on the properties of the compressible reservoir fluid.

## 30. (Original) The system of claim 28 wherein:

- the reservoir fluid is slightly compressible;
- the injection fluid is compressible or slightly compressible and contains desirable additives for compatibility with said formation; and
- the transformation of pressure measurement data is based on the properties of the slightly compressible reservoir fluid.